

# Computer reliability

## Laboratory exercise 1

### Reliability parameters of computers

**1.Goal:** To achieve knowledges about the general reliability parameters like success distribution, fault distribution, failure rate, density function, etc.

#### 2.Theoretical basics.

The main reliability characteristic is the **success distribution function**, or shortly **reliability**, which is equal to the probability of the reliable computer operation in the given time interval  $t$  by the given operation conditions

$$P(t) = W \{T > t\},$$

where  $T$  is time amount of the reliable system operation,  $W\{A\}$  is the probability of the event  $A$ . The opposite meaning function is **failure distribution function**, or shortly **unreliability**

$$Q(t) = W \{T \leq t\}.$$

From these function equations the next relations are followed directly

$$P(t) + Q(t) = 1, \\ 0 \leq P(t) \leq 1, \quad 0 \leq Q(t) \leq 1, \quad P(t_2) \leq P(t_1), \quad Q(t_2) \geq Q(t_1), \quad \text{where } t_2 > t_1.$$

In the reliability theory the systems are considered which satisfy the equations

$$P(0) = 1, \quad Q(0) = 0, \quad P(\infty) = 0, \quad Q(\infty) = 1,$$

i.e. these systems are operable at the initial time, and the operation time is finite one.

The determinant of the failure distribution function is the distribution density or shortly **density function**

$$f(t) = \frac{dQ(t)}{dt} = - \frac{dP(t)}{dt}.$$

The relative value of the density function is the **fault intensity function** or **failure rate**

$$\lambda(t) = \frac{f(t)}{P(t)}.$$

When taking the integral of the density function we derive the estimation of the success distribution as the following

$$P(t) = e^{-\int_0^t \lambda(t) dt}$$

If a system consists of 3 parts with the failure rates  $\lambda_1, \lambda_2, \lambda_3$ , and a system fails when any of the parts fails then the resulting failure rate of the system is

$$\lambda = \lambda_1 + \lambda_2 + \lambda_3.$$

Operation period to a fault is equal to the **mean time to failure**:

$$T_0 = \int_0^{\infty} t \cdot f(t) dt = \int_0^{\infty} P(t) dt .$$

if  $\lambda = \text{const}$  then

$$P(t) = e^{-\lambda t} ,$$

and as a result

$$T_0 = \int_0^{\infty} e^{-\lambda t} dt = \frac{1}{\lambda} .$$

The system reliability  $P(t/t_1)$  at the interval  $(t_1, t)$ , if the system till  $t_1$  was in the faultless operation is searched from the relation

$$P(t) = P(t_1) \cdot P(t/t_1)$$

Hence the **reliability of faultless operation at the interval  $(t_1, t)$**  is

$$P(t/t_1) = e^{-\int_{t_1}^t \lambda(t) dt} .$$

If  $\lambda = \text{const}$ , which is named as the **exponential fault distribution law**, or **constant hazard rate law** then  $P(t/t_1) = e^{-\lambda(t-t_1)}$ . In this situation the probability of the faultless operation is independent on the previous operation. It is true for a system without runout and consenscence, or when the time period is small.

The probability of the faultless operation for the time period  $t_0 \ll T_0$  by the exponential fault distribution law is equal to

$$P(t_0) = e^{-\lambda \cdot t_0} \approx 1 - \lambda t_0 .$$

Respectively the probability of a fault for a time period, or the **effective failure rate** is

$$\lambda_e = \frac{1 - P(t_0)}{t_0} .$$

The **guaranteed technical resource  $t_\gamma$**  with respect to the guaranteed probability  $\gamma$  is derived from the equation  $P(t_\gamma) = \gamma$ . By  $\lambda = \text{const}$  the equation is  $e^{-\lambda t_\gamma} = \gamma$  from which we derive  $t_\gamma = -T_0 \cdot \ln \gamma$ . Because the value  $\gamma$  is near 1 (for example,  $\gamma = 0,9$ ), then

$$t_\gamma = -T_0 \cdot \ln(1 - (1 - \gamma)) \approx (1 - \gamma) \cdot T_0 .$$

In the real world the exponential fault distribution law, or shortly E-law occurs rarely. Therefore, to estimate the reliability parameters of the real systems more complex laws are considered. The **diffused monotonous distribution (hazard) model**, or shortly **DM-model** is used for the systems which fault due to the wearing, corrosion, etc., and is described by the formulas

$$f(t) = \frac{t + \tau}{2v\tau\sqrt{2\pi\tau t}} e^{-\frac{(t-\tau)^2}{2v^2\tau t}} ,$$

$$P(t) = 1 - \int_0^t f(x) dx = 1 - \int_0^t \frac{x + \tau}{2vx\sqrt{2\pi\tau x}} e^{-\frac{(x-\tau)^2}{2v^2\tau x}} dx , \quad T_0 = \tau \left(1 + \frac{v^2}{2}\right) ,$$

where  $\tau$  is the **scale parameter** and  $v > 0$  is the shape parameter. Usually the variable substitution  $\frac{x-\tau}{v\sqrt{\tau x}} = u$  is used. Then  $du = \frac{x+\tau}{2vx\sqrt{\tau x}} dx$ , and the integration limits from 0 to t are substituted by limits from  $-\infty$  to  $\frac{t-\tau}{v\sqrt{\tau t}}$ . As a result, the formula is simplified as

$$P(t) = \Phi\left(\frac{t-\tau}{v\sqrt{\tau t}}\right), \text{ where } \Phi(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^x e^{-\frac{u^2}{2}} du.$$

**DN** is the **diffused nonmonotonous distribution model** which is used for the electronic systems, which fails from the oldness, electromigration, etc.:

$$f(t) = \frac{\sqrt{\tau}}{vt\sqrt{2\pi t}} e^{-\frac{(t-\tau)^2}{2v^2\tau t}}, \quad P(t) = \Phi\left(\frac{\tau-t}{v\sqrt{\tau t}}\right) - e^{2v^{-2}} \Phi\left(-\frac{\tau+t}{v\sqrt{\tau t}}\right), \text{ and } T_O = \tau.$$

**LN** is the **logarithmically normal distribution model** which is used for the electronic and electromechanic systems, which fail due to the weariness from the periodical loading stresses:

$$f(t) = \frac{1}{vt\sqrt{2\pi}} e^{-\frac{(\ln t - \ln \tau)^2}{2v^2}}, \quad P(t) = \Phi\left(\frac{\ln \tau - \ln t}{v}\right), \text{ and } T_O = \tau e^{\frac{v^2}{2}}.$$

**W** is the **Weibull hazard model**, which is used as the approximation of different density and reliability functions depending on the scale parameter  $\tau$  and shape parameter  $v$ :

$$f(t) = \frac{v}{\tau} \left(\frac{t}{\tau}\right)^{v-1} e^{-\left(\frac{t}{\tau}\right)^v}, \quad P(t) = e^{-\left(\frac{t}{\tau}\right)^v}, \quad \lambda(t) = \frac{v}{\tau} \left(\frac{t}{\tau}\right)^{v-1}, \quad T_O = \tau \Gamma\left(1 + \frac{1}{v}\right),$$

where  $\Gamma(x) = \int_0^{\infty} u^{x-1} e^{-u} du$  is the gamma function for  $x > 0$ .

### 3. Tasks

#### Task 1.

Consider a system consists of n processing units (PU) and it fails when n-k and more PUs fail. The failures are independent and have equal and independent failure rate  $\lambda = 10^{-4} \text{ hours}^{-1}$ .

**Build the following 2-d diagrams** of the argument  $\lambda t$  both for a single PU and for the whole system:

A1) success distribution function;

A2) failure distribution function;

A3) density function;

A4) failure rate;

A5) mean time to failure;

A6) reliability of faultless operation at the interval  $(\tau, t + \tau)$  if till the moment  $\tau = 10^4$  hours the system has operated without faults.

A7) reliability of faultless operation at the interval  $(\tau, t + \tau)$  if till the moment  $\tau$  m PUs had failed (a single PU is not considered).

**Estimate** the following numerical characteristics both of a single PU and of the whole system

B1) mean time to failure;

B2) effective failure rate;

B3) mean time to failure if a system (orPU) has operated  $\tau=10^4$  hours without faults.

B4) mean time to failure if a system (orPU) has operated  $\tau=10^4$  hours, and  $r$  PUs have failed.

B5) and B6) guaranteed technical resource  $t_\gamma$  with respect to the guaranteed probability  $\gamma=0.9$  and  $\gamma=0.99$ .

**Estimate** a number of additional PUs which are needed for

C1) decreasing  $\lambda_e$  in  $M$  times;

C2) increasing mean time to failure in 2 times.

## Task 2.

Perform all the points of the task 1 for the situation when the distribution function is not exponential but  $Q(t)$ : DM, DN, LN, or W.

## 4. Variant selection

The individual parameters for the tasks are selected in the following table

$C_5$	$n$	$Q(t)$	$\tau$ , hours	$\nu$	$C_4$	$M$	$C_3$	$K$	$C_2$	$m$	$r$
0	9	DM	6667	1	0	10	0	0	0	1	2
1	8	DN	$10^4$	1	1	100	1	1	1	2	1
2	7	LN	6075	1	2	1000	2	2	-	-	-
3	6	W	5000	0,5	3	10000	-	-	-	-	-
4	5	W	11077	1,5	-	-	-	-	-	-	-

where  $C_k$  is the remainder of division of the student's record book number to  $k$ .

For example, consider the record book number  $k=1234$ .

Then  $k = 246*5+4 = 308*4+2 = 411*3+1 = 617*2+0$ .

As a result,  $C_5 = 4$ ;  $C_4 = 2$ ;  $C_3 = 1$ ;  $C_2 = 0$ .

## 5. Example of the task solution

Consider a system of 8 PUs which fails when 6,7 or 8 PUs failed. The faults are independent on each other, and have equal and stable failure rate. Estimate the system reliability if a system has operated  $\tau$  hours without faults.

The reliability is derived from the formula

$$P_C(t+\tau) = P_C(\tau) \cdot P_C(t+\tau/\tau),$$

where  $P_C(t)$  is reliability of the system,  $P_C(t+\tau/\tau)$  is reliability to find.

Therefore, 
$$P_C(t+\tau/\tau) = \frac{P_C(t+\tau)}{P_C(\tau)}$$

Because the system fails when 6, 7, or 8 PUs fail, then

$$\begin{aligned} P_C(t) &= 1 - Q_C(t) = 1 - C_8^6 P^2 (1-P)^6 - C_8^7 P (1-P)^7 - (1-P)^8 = \\ &= 1 - (1-P)^6 (1+6P+21P^2), \end{aligned}$$

where  $P = e^{-\lambda t}$  is reliability of a single PU,  $C_m^n$  is a combination of  $n$  from  $m$ . The result is

$$P_C(t+\tau/\tau) = \frac{1 - (1-P(t+\tau))^6 (1+6P(t+\tau)+21P^2(t+\tau))}{1 - (1-P(\tau))^6 (1+6P(\tau)+21P^2(\tau))}$$

Consider the same system with the same conditions. Estimate the system reliability at the period from  $\tau$  to  $\tau+t$  hours if in the system which was operated  $\tau$  hours 2 PUs failed.

Because the failure rate is considered to be stable, then the system reliability doesn't depend on the time period till the moment  $\tau$ , but it depends on the interval  $(\tau, \tau+t)$ . Therefore the system will fail, when 6 and more PUs fail in it. But 2 PUs have already failed, and as a result, the system will fail if 4, 5, or 6 PUs fail. The resulting reliability is equal to

$$P_c(t) = 1 - C_6^4 P^2 (1-P)^4 - C_6^5 P (1-P)^5 - (1-P)^6 = 1 - 15P^2 (1-P)^4 - 6P (1-P)^5 - (1-P)^6.$$